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PRECISION MEASUREMENTS OF

MERCURY 198 WAVELENGTHS

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PRECISION MEASUREMENT OF MERCURY 198 WAVELENGTHS

A DISSERTATION

SUBMITTED TO THE SCHOOL OF GRADUATE STUDIES
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DEPARTMENT OF PHYSICS

by

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ABSTRACT

The vacuum wavelengths of eighteen lines of the Mercury 198 spectrum were measured. A Fabry-Perot interferometer with three different etalon spacers was used. The results agree within experimental error with measurements made by other experimenters, J.M. Blank, W.F. Meggers and K.G. Kessler, and K. Burns and K.B. Adams.

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I INTRODUCTION

Precision measurements in spectroscopy require that there be a standard wavelength (or wavelengths) to which subsequent investigation may be referred. Because it is not always convenient or even possible to use the primary standard, cadmium 6438.4696A, lines from the spectra of various other elements have been proposed as secondary standards; for example, many of the lines of neon and argon are used for this purpose.

In 1940 it was reported by Weins and Alvarez (1) that ¹⁹⁸₈₀ Hg could be excited to emit radiation free from isotopic and hyperfine structure. Furthermore it can be excited at low temperatures and low vapor pressure; hence the wavelengths are determinable to a high degree of accuracy, of the order of 1 part in 5×10^7 . Various experimenters^(2,3,4) have made measurements of these lines. In the present work these measurements are repeated with special emphasis on the ultra-violet portion of the spectrum.

The vacuum wavelengths were determined by means of a Fabry-Perot interferometer crossed with a Hilger E 1 Littrow Spectrograph. The measurements were made with respect to 4 neon visible lines as secondary standards.

II THEORY

1. Fabry - Perot Interferometer

The Fabry - Perot interferometer consists of a pair of transparent plates coated with a partially reflecting, partially transmitting layer of metal. The plates usually are glass, or quartz if the investigation is to be carried into the ultra-violet. The metals used are silver and aluminum because these possess the essential properties, namely, high reflectivity (80-95%) and low absorption, necessary to obtain high resolution with appreciable intensity. Silver is superior to aluminum in the infra-red and visible regions of the spectrum⁽⁶⁾ but it has a strong absorption band at 3000 Å; hence, for ultra-violet spectroscopy aluminum coated plates are essential. The reflectivity of aluminum begins to decrease considerably at about 2500 Å.

The plates of the interferometer are separated by a spacer which is often quartz or invar. These materials are chosen for their low coefficient of thermal expansion to insure stability throughout small temperature variations.

The components of the interferometer are assembled so that the plates are as nearly parallel as possible,

to an accuracy of a fraction of a wavelength of light. The spacer must be of a high quality so that such arrangement is attainable.

A ray of light entering the interferometer in a direction nearly perpendicular to the plates is partly reflected and partly transmitted at each metal surface (fig. 1). The condition for constructive interference is

$$p\lambda = 2\mu t \cos \theta \quad (1)$$

where p is an integer, λ is the wavelength of the light, θ is the angle of incidence, t is the plate separation, and μ is the refractive index of the medium between the plates. If the space between the plates is evacuated $\mu = 1$. Because of the symmetry about the normal to the plates circles of interference maxima and minima, focussed at infinity, will be observed.

2. Calculation of the Fractional Part of the Order Number

An order number P which in general will not be integral is assigned to the centre of the pattern (here $\theta = 0$); P may be written as the sum of an integer P_0 and a fraction e . Then at the centre of the interference pattern

$$(P_0 + e)\lambda = 2t \quad (2)$$

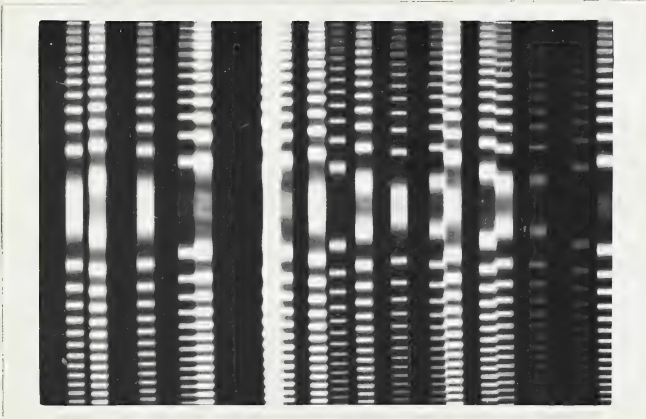


Plate 1. - Typical Interference Pattern

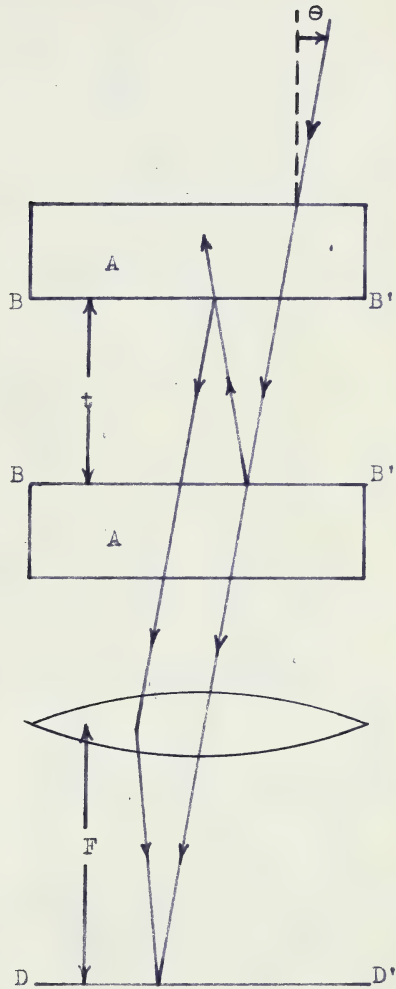


Figure 1. Ray of Light Passing Through Interferometer.

- A: etalon plates
- BB': metal surfaces
- C: convex lens
- DD': focal plane of lens

The order number of the n^{th} bright ring is $(P_0 - n)$ where $n = 0, 1, 2, \dots$, beginning at the centre of the pattern and counting outwards. Now

$$\cos \theta_n = 1 - \frac{D_n^2}{8f^2} \quad (3)$$

if $D_n \ll f$, where D_n is the diameter of the n^{th} bright ring as observed in the focal plane of the lens of focal length f . Substitution in equation (1) gives the result

$$2t \left(1 - \frac{D_n^2}{8f^2} \right) = (P_0 - n)\lambda$$

But from equation (2)

$$(P_0 + e)\lambda = 2t$$

$$\therefore e = \frac{2t}{8\lambda f^2} D_n^2 - n$$

$$\text{Or } e = K D_n^2 - n \quad (4)$$

where K is a constant independent of n .

The fractional portion of the interference order number at the centre of the pattern can be calculated from equation (4). To increase the accuracy of this calculation several diameters are measured and a least squares line is fitted to the data. The normal equations (Appendix I) are

$$je = K \sum_{n=0}^{j-1} D_n^2 - \sum_{n=0}^{j-1} n \quad (5)$$

$$e \sum_{n=0}^{j-1} n = K \sum_{n=0}^{j-1} n D_n^2 - \sum_{n=0}^{j-1} n^2 \quad (6)$$

where j is the number of diameters measured. These

equations may be solved for e and K

$$e = \frac{\sum_{n=0}^{j-1} n^2 \sum_{n=0}^{j-1} D_n^2 - \sum_{n=0}^{j-1} n \sum_{n=0}^{j-1} n D_n^2}{j \sum_{n=0}^{j-1} n D_n^2 - \sum_{n=0}^{j-1} n \sum_{n=0}^{j-1} D_n^2} \quad (7)$$

$$K = \frac{j \sum_{n=0}^{j-1} n - \left(\sum_{n=0}^{j-1} n \right)^2}{j \sum_{n=0}^{j-1} n D_n^2 - \sum_{n=0}^{j-1} n \sum_{n=0}^{j-1} D_n^2} \quad (8)$$

In particular for $j = 5$ these equations become

$$e = \frac{3 \sum_{n=0}^4 D_n^2 - \sum_{n=0}^4 n D_n^2}{\frac{1}{2} \sum_{n=0}^4 n D_n^2 - \sum_{n=0}^4 D_n^2} \quad (9)$$

$$K = \frac{1}{2 \left(\frac{1}{2} \sum_{n=0}^4 n D_n^2 - \sum_{n=0}^4 D_n^2 \right)} \quad (10)$$

An estimate of the accuracy of the value of e is made by computing the standard error of estimate.

$$\text{Standard error of estimate} = \sqrt{\sum_{n=0}^4 \frac{(e - e_n)^2}{5}} \quad (11)$$

where e_n is computed from equation (4).

A more detailed and complete theory of the Fabry-Perot interferometer is given by Meissner⁽⁵⁾ and Tolansky.⁽⁶⁾

3. Calculation of Etalon Separation.

The separation of the interferometer plates must be known to about 1 part in 10^8 if an unknown wavelength is to be calculated to that order of accuracy. To find the separation a standard wavelength (or wavelengths) is measured; secondary standards such as the lines of neon are convenient for this purpose. For the calculation of the separation it is necessary to know:

- 1) The wavelengths of at least two of the standard lines to an accuracy of about 1 part in 10^8 .

- 2) The fractional parts of the order numbers of the standard lines.
- 3) An approximate value of the separation (preferably to at least four significant figures).

With two calculating machines the following method may be used to compute the precise value of the separation. An approximate value of P (the interference order number) is computed from equation (2) for two wavelengths, using the exact value of the wavelengths and the approximate value of $2t$. The two wavelengths are then set on the calculating machines as constant multiplicands; the order numbers with the measured fractional parts are set on the keyboards as multipliers. Multiplication will give two values of $2t$ which will probably be different from each other. The integral parts of the order numbers are changed by constant amounts and the multiplications are continued until the two calculated values of $2t$ agree with each other to about 1 part in 10^8 . A third and fourth wavelength are used as a check.

It is usually necessary to follow this procedure only once since the value of $2t$ does not change appreciably for subsequent exposures with the same etalon spacer.

Several other methods of calculating the plate separation are discussed by Meissner.⁽⁵⁾

4. Calculation of Wavelengths.

To calculate the value of an unknown wavelength it is necessary to know:

- 1) The fractional part of P for the unknown wavelength.
- 2) An approximate value of the wavelength (5 or 6 significant figures)
- 3) An exact value of $2t$ (about 1 part in 10^8).

By equation (2) an approximate value of P is calculated from the exact value of $2t$ and the approximate wavelength. The measured fractional part is substituted into P and equation (2) is used again to calculate an exact value of the wavelength.

The known approximate value of the wavelength may not be sufficient to determine the integral part of P exactly; as a result P may be incorrect by the amount of some small integer. In this case the observations at a different etalon separation serve as a check and the correct integral portion of the order number is readily established.

5. Phase Change at Reflection.

Upon reflection at a metallic surface a small phase change is introduced between the incident and reflected beams of light. This phase change is a function of the wavelength of the incident light, of the nature of the metal, its thickness and condition. To eliminate the dispersive effect that the phase change has on the cal-

culated values of the wavelength it is necessary to make a correction to each wavelength. With observations made at at least two different etalon separations, it is possible to determine the necessary correction experimentally.

The phase change correction can be made by assuming an apparent change δt in the separation of the etalon plates, and independent of the separation. For two thicknesses t_1 and t_2 equation (2) may be written

$$p' = \frac{2t_1}{\lambda'} = \frac{2(t_1 + \delta t)}{\lambda} \quad (12)$$

$$p'' = \frac{2t_2}{\lambda''} = \frac{2(t_2 + \delta t)}{\lambda} \quad (13)$$

where λ' and λ'' are the observed wavelengths at thicknesses t_1 and t_2 , respectively, and λ is the true wavelength. The solutions for λ are

$$\lambda = \lambda' + \frac{(\lambda'' - \lambda')t_2}{t_2 - t_1} \quad (14)$$

$$\lambda = \lambda'' + \frac{(\lambda'' - \lambda')t_1}{t_2 - t_1} \quad (15)$$

The choice of etalon spacers is important; choosing two nearly equal separations makes the factors $(\frac{t_2}{t_2 - t_1})$ and $(\frac{t_1}{t_2 - t_1})$ large. The error in the wavelength difference $(\lambda'' - \lambda')$ is multiplied by these factors, and hence the error in the phase change corrections will be proportional to them. It is desirable to use at least one large and one small etalon separation.

K.W. Meissner⁽⁵⁾ describes more fully this method of applying a correction for phase change; also, A.W. Smith⁽⁷⁾ outlines another method.

III APPARATUS

1. General Considerations

The apparatus used in the work was the same, with some minor alterations, as that used by A.W. Smith⁽⁷⁾ and R.A. Olafson.⁽⁸⁾ A more detailed account of some aspects of the apparatus is given by them.

The Fabry - Perot interferometer used consisted of two quartz plates each aluminized on one surface. The spacers which were available were made of invar. To separate the many lines of the neon and mercury spectra it was necessary to "cross" the interferometer with a spectrograph. The methods of doing this are discussed by Tolansky.⁽⁶⁾

The spectrograph used for this purpose was a Hilger El Littrow Spectrograph with quartz optical components. It was found necessary to redetermine the settings which best focus horizontal lines; the results are given in Appendix II. The entrance slit was opened about $\frac{1}{2}$ mm.

The etalon was situated in a vacuum-tight brass chamber which in turn was immersed in a water bath. The temperature of the bath was thermostatically controlled; a heating element, water-cooled coils, and a stirring mechanism assured that the temperature of the bath was kept constant. By varying the rates of heating and cooling it was found possible to control the length



Plate 2. Components of Interferometer.

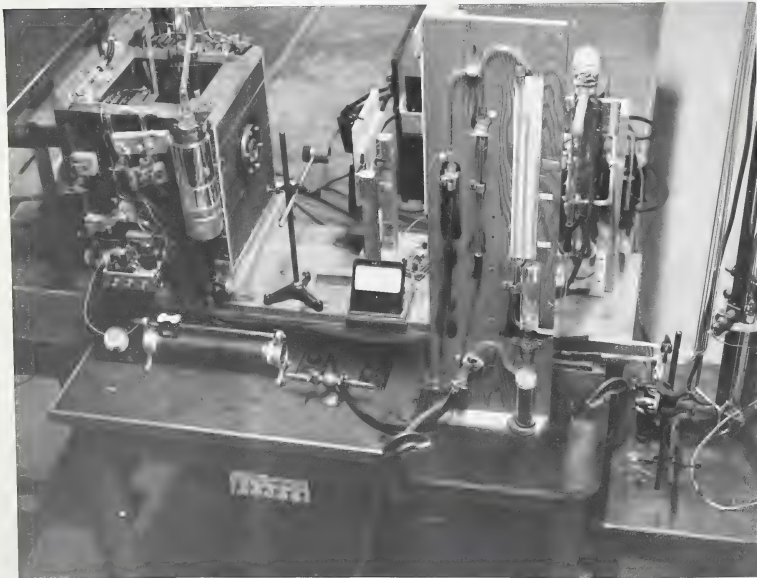


Plate 3. General View of Apparatus.

of the thermostatic cycle. This was adjusted to about 4 minutes, the same length of time as the duration of the neon and shortest mercury exposures. In this way the average temperature during the exposure would be the same as the average temperature over a thermostatic cycle.

A check was kept on the temperature by means of a Beckman thermometer. This instrument was calibrated, but since the temperature does not enter directly into any calculations, only the results of that calibration will be given here:

$$T (\pm .006 ^\circ \text{C}) = 17.054 ^\circ \text{C} + 1.015 B$$

where T is the temperature in degrees centigrade and B is the reading of the Beckman thermometer. The method of calibration was the same as that used by A.W. Smith⁽⁷⁾ and R.A. Olafson.⁽⁸⁾ The average temperature of the bath for each exposure was $21.40 ^\circ \text{C}$.

The thermometer showed variations of $.01 ^\circ \text{C}$ about the average temperature during one thermostatic cycle. Taking the coefficient of thermal expansion of invar to be $0.9 \times 10^{-6} / ^\circ \text{C}$,⁽⁹⁾ this results in a variation of 2×10^{-8} cm. in the length of the etalon spacer. Since this variation is about 1/10 the uncertainty in the measurement of the etalon separation, it may be neglected.

The mechanical vacuum pump used to evacuate the

the etalon chamber was situated at a distance from the main apparatus and mounted on three sets of shock mountings. This permitted continuous pumping of the chamber without the danger of excessive vibration throughout the exposures. The mechanical pump was connected to a mercury diffusion pump with 10 meters of 14 mm. diameter pyrex tubing. A dry ice-methanol trap was built into the vacuum system at the entrance to the etalon chamber; this trap prevented mercury and water vapor from entering the chamber.

The air pressure in the etalon chamber was measured with a MacLeod gauge. While the pressure was not measured accurately, it was found to be less than one micron of mercury. At that pressure the residual air would produce a change of 0.000002 Å at the most in the wavelengths at 6000 Å and less in the ultra-violet. Since this is considerably beyond the accuracy of measurement of the wavelengths, the effect of the residual pressure may be neglected.

2. Sources and Excitation.

The neon source was an ordinary Geissler discharge tube. The effective size of the source was limited by an aperture of black paper fitted on the capillary portion of the tube. The tube was excited by 60 cycle, 110 volts transformed to a potential of 8000 volts. The current through the tube was 7 milliamperes.

The mercury 198 tube was supplied by Baird Associates, Cambridge, Massachusetts. It was constructed of vycor glass and contained a few milligrams of artificially prepared $^{198}_{80}\text{Hg}$ and a trace of $^{199}_{80}\text{Hg}$. A 600 megacycle/sec. war-surplus radar generator was used to excite the discharge. The generator has two triode push-pull, tuned plate-tuned cathode oscillators working in parallel. A detailed description is given by M.I.T. Radar School Staff.⁽¹⁰⁾ According to Tolansky⁽⁶⁾ no clean-up of the element in the tube occurs under the electrodes; therefore the tube was wrapped completely in aluminum foil except for the interelectrode space.

3. The Optical System

The light from the discharge tubes, which were viewed transversely (i.e., in a direction perpendicular to their long axis), was condensed by a quartz lens and focussed at a spot approximately halfway between the etalon plates (fig. 2). The discharge tubes were fastened to a sliding holder which allowed them to be alternately positioned in front of the condensing lens. After emerging from the interferometer the light was focussed on the slit of the spectrograph by a quartz-fluorite achromat of focal length 26 cm.

To check that the centre of the interference pattern fell on the slit a small light source was placed in the spectrograph near the prism. The light

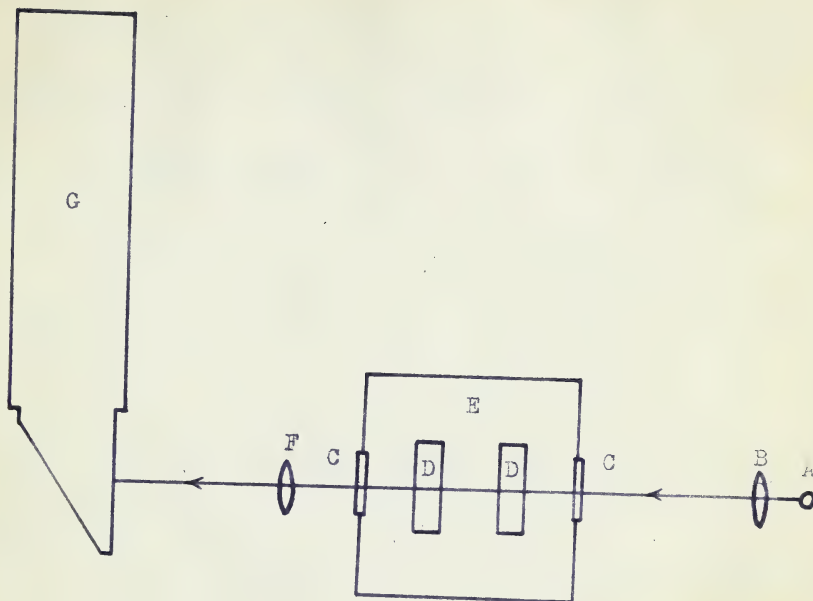


Figure 2. Optical System

- A: discharge tube
- B: quartz condensing lens
- C: optically flat quartz windows
- D: etalon plates
- E: etalon chamber
- F: quartz-fluorite achromat
- G: Hilger E 1 Spectrograph

from this source was directed through the slit to the etalon plate and reflected back from the metal surface towards the slit. The etalon was considered perpendicular to the path of the light beam when the reflected light fell back exactly on the slit.

4. The Densitometer.

Analysis of the interference patterns involved the measurement of the distance between corresponding fringes on opposite sides of the centre of the pattern. A densitometer was used to make a trace of the pattern on a paper chart. An ordinary scale was then used to make the necessary measurements.

The densitometer consists essentially of a plate holder moving on a carriage and a device for detecting variations in the image density of the photographic emulsion. The carriage screw which was known to be of high quality, was rotated by the external drive of the Esterline - Angus recording milliammeter. A slight change was made in the method of driving the carriage screw. Previously the chart drive and the carriage drive had been connected by a set of fiber gears. Since it was thought that these gears might have small irregularities, an alteration was made so that the carriage and chart^{were} driven from the same shaft. No conclusion could be made as to the consequences of this change, but indications were that the trace of

the pattern was more uniform.

The device for scanning the pattern consisted of a light focussed on the photographic emulsion; from there the light was focussed by another lens on the slit of a photomultiplier tube 931-A. The output of the photomultiplier tube was fed into a 6J5 triode used as a cathode-follower amplifier; the current of this amplifier was measured with the Esterline-Angus recording milliammeter.

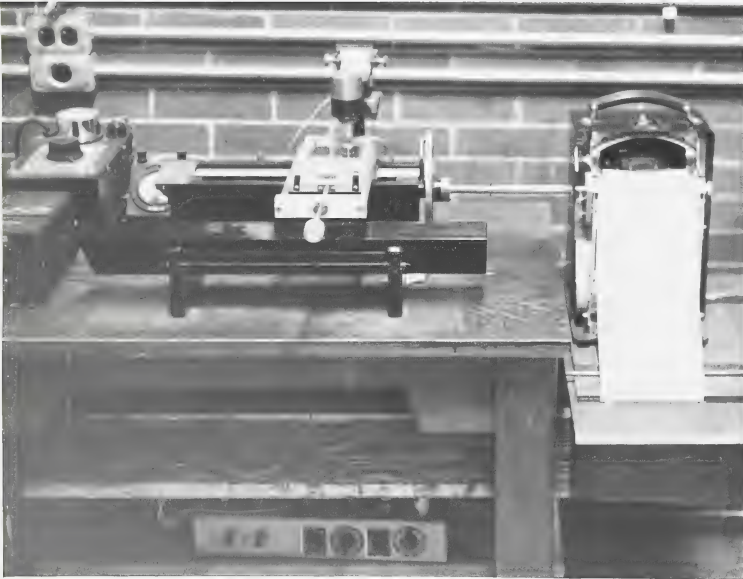


Plate 4. Densitometer.

IV EXPERIMENTAL PROCEDURE

1. Preliminary Adjustments

Several hours before the exposure was begun the temperature control for the water bath was put into operation to permit the etalon to reach temperature equilibrium. After equilibrium had been reached the etalon was checked for parallelism of the plates. This was done by moving a telescope focussed at infinity from side to side and up and down across the face of the etalon plate. If the plates were parallel no difference in the diameter of the interference rings was observed when this was done. In a few cases a slight adjustment was necessary to bring the plates back to parallelism.

After the check for parallelism the etalon chamber was flushed twice with air which had been passed over phosphorus pentoxide^x and anhydrous sodium hydroxide in order to remove water vapor and carbon dioxide. Finally the chamber was evacuated and the diffusion pump was left in operation for at least one hour before the exposures were begun. After this time the air pressure had been reduced sufficiently and temperature equilibrium had certainly been reached.

2. Vacuum Exposures.

The vacuum exposures were then made on Eastman

Kodak III-F Spectroscopic Plates, which are sensitive from 2000 A to 6900 A, in the following order:

- 1) Neon, visible, 4 minutes.
- 2) Mercury, visible, 30 minutes.
- 3) Mercury, far ultra-violet, 4 minutes.
- 4) Mercury, ultra-violet, 90 minutes.
- 5) Neon, visible, 4 minutes.

The temperature and the functioning of the thermostat were checked after each exposure to insure that the temperature had been maintained constant. The air pressure was also checked.

Nine plates were taken, three with each of the etalon spacers.

3. Processing of Plates.

Kodak

The spectroscopic plates were developed in D-19 for 8 to 9 minutes depending on the condition of the developer, and fixed in Ansco acid fixer with hardener for 10 minutes. Care was taken to have the developer, fixer and wash water at nearly the same temperature. Finally the plates were washed, rinsed in a wetting agent, and dried in a gentle stream of unheated air blown through oil-soaked cheesecloth to collect the dust from the air. These precautions are necessary to prevent shrinking or expansion of the emulsion during the processing. (6) (13)

V RESULTS AND DISCUSSION

Observations were made with three etalon spacers, 1.5 cm., 2.5 cm., and 2.8 cm. Since no large spacers other than the 1.5 cm. and 2.8 cm. were available, the 2.5 cm. spacing was obtained by placing 1.0 cm. and 1.5 cm. spacers together. The two spacers together tended to be somewhat more unstable than a single spacer. Whereas the single spacers changed about 1 part in 10^8 during the 3 hours necessary for the exposures, the double spacer changed about 4 parts in 10^8 during that time. Nevertheless since this change was of the order of the accuracy possible in the measurement of the plate separation, the results from all three spacers were given equal value.

The data from the nine plates is given in Appendix IV. Four neon lines which had been measured with respect to the primary standard, cadmium 6438.4696 Å, were chosen as the secondary standards.⁽⁹⁾ The standard wavelengths were converted to vacuum wavelengths by use of the refractive index calculated from the averaged data of Barrell and Sears and of Perard (Appendix III). Eighteen lines of the mercury 198 spectra were measured. Seventeen of these were from mercury in the ground and singly-ionized state; one, the 4705 Å line was from the spectrum of doubly-ionized mercury.

Phase change corrections were made by combining the data from the 1.5 cm. and 2.5 cm. and from the 1.5 cm. and 2.8 cm. spacers. The calculations are given in Appendix IV. The corrected wavelengths calculated from the two combinations were averaged to give final values of wavelength. These are shown in Table 1; the standard wavelength is calculated by using the refractive index computed from the averaged data of Barrell and Sears and of Perard. The experimental errors quoted are the standard deviations.

Table 1.

Final Vacuum Wavelengths of Mercury 198

| Final Vacuum Wavelength (in Angstroms) | Refractive Index $(\mu - 1) \times 10^6$ | Standard Air Wavelength |
|--|--|----------------------------|
| 2537.26830 ±.00028 | 300.65 | 2536.50571 |
| 2652.83253 37 | 297.87 | 2652.04257 |
| 2753.59686 45 | 295.77 | 2752.78266 |
| 2894.44652 28 | 293.27 | 2893.59793 |
| 2968.14968 23 | 292.15 | 2967.28280 |
| 3022.37973 15 | 291.33 | 3021.49947 |
| 3024.35686 38 | 291.30 | 3023.47611 |
| 3126.57562 31 | 289.95 | 3125.66932 |
| 3342.44273 24 | 287.55 | 3341.48189 |
| 3651.19636 54 | 284.91 | 3650.15639 |
| 3655.88053 33 | 284.88 | 3654.83935 |
| 3664.32416 31 | 284.82 | 3663.28080 |
| 4047.71484 33 | 282.45 | 4046.57188 |
| 4078.98951 44 | 282.29 | 4077.83838 |
| 4359.56218 44 | 281.01 | 4358.33746 |
| 4705.95714 130 | 279.64 | 4704.64152 |
| 5462.27094 51 | 277.85 | 5460.75368 |
| 5792.26810 48 | 277.25 | 5790.66263 |

Table 2. Comparison of Results with Other Experimenters.

| Standard Wavelength* (in Angstroms) | Present Work** | J.M. Blank ⁽²⁾ | W.F. Meggers and K.G. Kessler ⁽³⁾ | K.Burns and K.B.Adams ⁽⁴⁾ |
|--|----------------|---------------------------|---|---|
| 2536 | .5057 ±.0003 | | .5064 | .5063 |
| 2652 | .0426 4 | | .0426 | .0425 |
| 2752 | .7827 4 | | .7827 | .7828 |
| 2893 | .5979 3 | | .5980 | .5982 |
| 2967 | .2828 2 | | .2833 | .2832 |
| 3021 | .4995 2 | | .4997 | .4996 |
| 3023 | .4761 4 | | .4762 | .4764 |
| 3125 | .6693 3 | | .6700 | .6698 |
| 3341 | .4819 2 | | .4814 | .4814 |
| 3650 | .1564 5 | .15688 | .1567 | .1564 |
| 3654 | .8394 3 | | .8393 | .8392 |
| 3663 | .2808 3 | | .2808 | .2808 |
| 4046 | .5719 3 | .57161 | .5715 | .5712 |
| 4078 | .8384 4 | | .8379 | .8379 |
| 4358 | .3375 4 | .33763 | .3376 | .3372 |
| 4704 | .6415 13 | — | — | — |
| 5460 | .7537 5 | .75313 | .7532 | .7532 |
| 5790 | .6626 5 | .66272 | .6626 | .6626 |

* Integral part only

** Columns 2, 3, 4 and 5 contain the fractional part of the wavelength only.

A comparison of the results of the present work with those of previous experimenters is made in Table 2. There is agreement within experimental error for most of the wavelengths. Exceptions are the lines 2537 A, 3126 A, and 3341 A. For these lines the phase change correction as calculated from the 1.5 cm. and 2.5 cm. spacer combination is considerably different from that calculated from the 1.5 cm. and 2.8 cm. spacer combination; since the two combinations are nearly the same, the phase change corrections should also be nearly the same. However this consideration cannot be used as a basis for rejecting the results for these lines. The two phase change corrections differ considerably also for several other lines which do agree well with previous determinations, namely, the lines 3655 A, 3663 A, 4358 A, and 5791 A.

The largest part of the error in calculation is introduced during the application of the phase change correction. As was mentioned previously in the theory of the phase change correction, this error can be kept at a minimum by a proper choice of etalon separations. It would appear that a 0.5 cm. or 1.0 cm. spacer would have been a better choice than the 1.5 cm. spacer. In those cases the probable error in the correction would have been one-third or one-half that of the present work.

Since the lines of the mercury discharge are very sharp, a greater accuracy in measurement should be attainable - J.M. Blank ⁽²⁾, for instance, quotes a standard deviation of

about 0.0001 Å in his determination of the wavelengths. A place for possible improvement exists in the measurement of the fractional part of the order number, e . The criterion for accepting the measured value of e was arbitrarily taken to be that the standard error of estimate should be less than 0.0075. It was possible to achieve this accuracy, with one or two exceptions. In many cases it was found that the accuracy was improved by a remeasurement of line; hence it would appear that the manner in which the densitometer itself was operated had some effect on the results of the measurement. The best results were obtained from the more intense lines; the lower limit on the standard error of estimate for these lines appeared to be 0.0010, with most being around 0.0030. It is likely that the values of e would be improved if each line were measured three times, say, and the average result taken.

Appendix 1. Derivation of Normal Equations For
The Least Squares Method.

The least squares method provides a useful criterion for computing the best equation relating sets of experimental data.

For an equation of the form

$$y = a + bx + cx^2 + \dots \quad (1)$$

there will be values of Y_{cn} corresponding to values of X_n , where Y_{cn} is computed by the equations

$$\begin{aligned} Y_{c1} &= a + bX_1 + cX_1^2 + \dots \\ Y_{c2} &= a + bX_2 + cX_2^2 + \dots \\ &\dots \\ Y_{cN} &= a + bX_N + cX_N^2 + \dots \end{aligned} \quad (2)$$

The criterion of the least squares method is that the quantity $\sum_{n=1}^N (Y_n - Y_{cn})^2$ be a minimum, where Y_n is the experimental value of the first set corresponding to the value of X_n of the second set. Application of the criterion results in the equations

$$\begin{aligned} \frac{\partial}{\partial a} \sum_{n=1}^N (Y_n - Y_{cn})^2 &= 0 = 2 \sum_{n=1}^N (Y_n - a - bX_n - cX_n^2 - \dots) \\ \frac{\partial}{\partial b} \sum_{n=1}^N (Y_n - Y_{cn})^2 &= 0 = 2 \sum_{n=1}^N (Y_n - a - bX_n - cX_n^2 - \dots) X_n \\ &\dots \end{aligned} \quad (3)$$

Or, rewriting,

$$\begin{aligned} \sum_{n=1}^N Y_n &= Na + b \sum_{n=1}^N X_n + c \sum_{n=1}^N X_n^2 + \dots \\ \sum_{n=1}^N X_n Y_n &= a \sum_{n=1}^N X_n + b \sum_{n=1}^N X_n^2 + c \sum_{n=1}^N X_n^3 + \dots \end{aligned} \quad (4)$$

Equations (4) are the normal equations.

A measure used to indicate the excellence of fit of the least squares equation is the standard error of estimate; it is computed by the relation

$$\text{Standard error of estimate} = \sqrt{\frac{\sum_{n=1}^N (Y_n - Y_{cn})^2}{n}} \quad (5)$$

Appendix 2. Focus Settings of the Hilger Spectrograph

The focus settings of the Hilger El Littrow Spectrograph are not the same for focussing horizontal and vertical lines because of astigmatism in the spectrograph. Since the interference maxima appear as horizontal lines across the slit, settings must be determined which best focus such lines.

For each region of the spectrum the two foci for horizontal and vertical lines are closest to each other for the longer wavelengths. For example, in the region 3400 A - 7000 A the foci are closest together at 7000 A; in the region 2400 A - 3400 A the foci are closest at 3400 A. The foci are considerably closer together for the 3400 A line in the 2400 A - 3400 A region than for that line in the 3400 A - 7000 A region.

The line 2537 A shows appreciable lateral spreading in the region 2400 A - 3400 A; as a result there is an apparent decrease in intensity and the line is diffused. Settings were found for a region 2700 A and less; in that region the 2537 A line appeared much sharper and a shorter exposure was required.

The focus settings were found by test exposures. A brass slide across which were placed a number of fine glass strands was substituted for the fishtail. When the slide was in position the glass strands were very nearly in contact with the spectrograph slit and acted

effectively as sharp horizontal lines. The results are summarized in the table.

| Region | Focus | Prism Rotation | Plate Holder Tilt |
|--------------------|--------|-------------------|-------------------------|
| 2400 A and less | 24 -17 | 12.00 | 16.0 |
| 2400 A- 3400A | 37 -6 | 14.83 | 13.3 |
| 3400 A- 7000A | 53-15 | 18.03 | 5.5 |

Appendix 3. Refractive Index of Air

The refractive index of air must be known to about 8 or 9 significant figures in order to convert the known standard wavelengths to vacuum wavelengths. The averaged data of Barrell and Sears (11) and of Perard (12) was used. A least squares line of the form

$$\mu - 1 = A + \frac{B}{\lambda^2} + \frac{C}{\lambda^4} \quad (1)$$

was fitted to their data, where A, B, and C are constants. The result is the equation

$$(\mu - 1) \times 10^6 = 272.670 + \frac{1.47353}{\lambda^2} + \frac{0.021010}{\lambda^4}$$

where λ is measured in microns.

The refractive index for the 4 neon lines used as secondary standards are given in the table.

| Standard Wavelengths (in Angstroms) | $(\mu - 1) \times 10^6$ | Vacuum Wavelengths |
|--|-------------------------|--------------------|
| 5852.4878 | 277.146 | 5854.10979 |
| 5944.8340 | 277.003 | 5946.48074 |
| 6217.2812 | 276.616 | 6219.00100 |
| 6266.4952 | 276.552 | 6268.22821 |

Appendix 4. Observations and Calculations

a. Observations from Vacuum Plates

The observations at the three etalon separations are summarized in tables 1, 2, and 3. The wavelengths which appear in tables 4 and 5 are the weighted averages of the wavelengths calculated in tables 1, 2, and 3. The standard errors of estimate, which are quoted in the tables, were used as a basis for determining the value of a calculation. In no case was any measurement given a weight of more than two as compared to one for the least accurate measurement.

Table 1. Data From 1.5 cm. Spacer.

| | Vacuum Wavelength (in Angstroms) | Interference Order Numbers* | Plate 1 | | Plate 2 | | Plate 3 | |
|-----------------------|---------------------------------------|-----------------------------|-----------------------------|---------------------------------------|-----------------------------|---------------------------------------|-----------------------------|---------------------------------------|
| | | | Interference Order Number** | Double Plate Separation (in cm.) | Interference Order Number** | Double Plate Separation (in cm.) | Interference Order Number** | Double Plate Separation (in cm.) |
| Initial Neon Exposure | 5854.10979 | 51,244 | .7506 | 2.99992 396 | .7576 | 2.99992 437 | .7559 | 2.99992 427 |
| | 5946.48074 | 50,448 | .7311 | 408 | .7375 | 446 | .7325 | 416 |
| | 6219.00100 | 48,238 | .0336 | 379 | .0373 | 402 | .0305 | 360 |
| | 6268.22821 | 47,859 | .2031 | 407 | .2033 | 408 | .2020 | 400 |
| | | | Average: | | Average: | | Average: | |
| | | | 2.99992 | 398 | 2.99992 | 424 | 2.99992 | 401 |
| Final Neon Exposure | 5854.10979 ^m | 51,244 | .7573 | 2.99992 435 | .7616 | 2.99992 461 | .7566 | 2.99992 431 |
| | 5946.48074 | 50,448 | .7346 | 429 | .7345 | 428 | .7354 | 433 |
| | 6219.00100 | 48,238 | .0328 | 374 | .0371 | 401 | .0318 | 368 |
| | 6268.22821 | 47,859 | .1985 | 378 | .2002 | 389 | .1991 | 382 |
| | | | Average: | | Average: | | Average: | |
| | | | 2.99992 | 404 | 2.99992 | 420 | 2.99992 | 403 |
| | | | Overall average: | | Overall average: | | Overall average: | |
| | | | 2.99992 | 404 | 2.99992 | 422 | 2.99992 | 402 |
| | Vacuum Wavelengths* (in Angstroms) | Interference Order Number* | Interference Order Number** | Vacuum Wavelength** (in Angstroms) | Interference Order Number** | Vacuum Wavelength** (in Angstroms) | Interference Order Number** | Vacuum Wavelength** (in Angstroms) |
| | | | | | | | | |
| Mercury Exposure | 2537 | 118,234 | .3938 ±.0048 | .26848 | .3838 ±.0046 | .26888 | .3865 ±.0052 | .26865 |
| | 2652 | 113,083 | .7818 29 | .83311 | .7913 40 | .83308 | .7812 39 | .83314 |
| | 2759 | 108,945 | .6340 40 | .59728 | .6563 60 | .59690 | .6220 39 | .59759 |
| | 2894 | 103,644 | .1445 35 | .44621 | .1457 46 | .44638 | .1354 23 | .44647 |
| | 2967 | 101,070 | .5222 32 | .14931 | .5272 22 | .14937 | .5143 33 | .14956 |
| | 3022 | 99,257 | .0236 55 | .37958 | .0306 29 | .37958 | .0202 50 | .37969 |
| | 3024 | 99,192 | .1015 28 | .35775 | .1236 36 | .35729 | .1033 56 | .35771 |
| | 3126 | 95,949 | .2061 17 | .57512 | .2103 35 | .57521 | .1976 66 | .57541 |
| | 3342 | 89,752 | .4675 09 | .44182 | .4682 25 | .44203 | .4692 41 | .44177 |
| | 3651 | 82,162 | .7874 51 | .19552 | .7886 19 | .19572 | .7719 53 | .19622 |
| | 3655 | 82,057 | .5235 32 | .87929 | .5248 33 | .87949 | .5170 22 | .87960 |
| | 3664 | 81,868 | .4276 18 | .32347 | .4261 13 | .32380 | .4278 42 | .32348 |
| | 4047 | 74,114 | .0328 41 | .71390 | .0367 26 | .71397 | .0239 24 | .71440 |
| | 4078 | 73,545 | .7790 58 | .98869 | .7895 31 | .98840 | .7724 55 | .98907 |
| | 4359 | 68,812 | .5049 19 | .56228 | .5143 26 | .56199 | .4982 24 | .56272 |
| | 4705 | 63,747 | .3706 39 | .95725 | .3602 36 | .95835 | .3638 56 | .95777 |
| | 5462 | 54,920 | .8164 27 | .27133 | .8254 10 | .27082 | .8226 30 | .27073 |
| | 5792 | 51,791 | .8755 29 | .26757 | .8769 35 | .26782 | .8793 15 | .26717 |

*Integral part only.

**Fractional part only.

Table 2. Data From The 2.5 cm. Spacer.

| | Vacuum Wavelengths (in Angstroms) | Interference Order Number* | Plate 4 | | Plate 5 | | Plate 6 | |
|-----------------------|--------------------------------------|----------------------------|-----------------------------|------------------------------------|-----------------------------|------------------------------------|---------------------------------|------------------------------------|
| | | | Interference Order Number** | Double Plate Separation (in cm.) | Interference Order Number** | Double Plate Separation (in cm.) | Interference Order Number** | Double Plate Separation (in cm.) |
| Initial Neon Exposure | 5854.10979 | 85,412 | 1.0225 | 5.00017 211 | .9863 | 5.00016 999 | .9876 | 5.00017 007 |
| | 5946.48074 | 84,086 | .2336 | 169 | .1997 | 967 | .2156 | 062 |
| | 6219.00100 | 80,401 | .5293 | 191 | .4972 | 991 | .5001 | 010 |
| | 6268.22821 | 79,770 | .1038 | 215 | .0703 | 5.00017 005 | .0781 | 054 |
| | | | | Average: 5.00017 196 | | | Average: 5.00016 990 | Average: 5.00017 033 |
| Final Neon Exposure | 5854.10979 | 85,412 | 1.0157 | 5.00017 171 | .9901 | 5.00017 022 | .9895 | 5.00017 018 |
| | 5946.48074 | 84,086 | .2292 | 142 | .2063 | 006 | .2085 | 019 |
| | 6219.00100 | 80,401 | .5220 | 146 | .4979 | 5.00016 996 | .4979 | 5.00016 996 |
| | 6268.22821 | 79,770 | .1016 | 201 | .0752 | 5.00017 036 | .0749 | 5.00017 034 |
| | | | | Average: 5.00017 165 | | | Average: 5.00017 015 | Average: 5.00017 017 |
| | | | | Overall average: 5.00017 181 | | | Overall average: 5.00017 003 | Overall average: 5.00017 025 |
| | Vacuum Wavelength* | Interference Order Number* | Interference Order Number** | Vacuum Wavelength** (in Angstroms) | Interference Order Number** | Vacuum Wavelength** (in Angstroms) | Interference Order Number** | Vacuum Wavelength** (in Angstroms) |
| | (in Angstroms) | Number* | Number** | (in Angstroms) | Number** | (in Angstroms) | Number** | (in Angstroms) |
| Mercury Exposure | 2537 | 197,069 | .0756 ±.0030 | .26862 | 1.9970 ±.0025 | .26873 | .0028 ±.0044 | .26876 |
| | 2652 | 188,484 | .2127 52 | .83322 | .1635 140 | .83297 | .1977 67 | .83260 |
| | 2753 | 181,586 | .9011 60 | .59719 | ----- | ----- | .8367 128 | .59731 |
| | 2894 | 172,750 | .5214 56 | .44672 | .4531 67 | .44684 | .4909 50 | .44633 |
| | 2968 | 168,460 | .9078 55 | .14963 | .8420 74 | .14973 | .8624 60 | .14950 |
| | 3022 | 165,438 | .2364 36 | .37978 | .1668 37 | .37998 | .1869 27 | .37974 |
| | 3024 | 165,330 | .0543 31 | .35745 | ----- | ----- | .0193 30 | .35714 |
| | 3126 | 159,924 | .8698 42 | .57551 | .7971 67 | .57582 | .8125 51 | .57565 |
| | 3342 | 149,596 | .3355 53 | .44271 | .2861 50 | .44262 | .3033 40 | .44239 |
| | 3651 | 136,946 | .1287 31 | .19617 | .0738 31 | .19634 | .0991 18 | .19582 |
| | 3655 | 136,770 | .6747 40 | .88005 | .6146 28 | .88035 | .6312 12 | .88007 |
| | 3664 | 136,455 | .5008 15 | .32411 | .4435 28 | .32434 | .4609 32 | .32403 |
| | 4047 | 123,530 | .7440 44 | .71448 | .6954 17 | .71463 | .7081 33 | .71439 |
| | 4078 | 122,583 | .5970 45 | .98930 | ----- | ----- | .5694 03 | .98895 |
| | 4359 | 114,694 | .3448 20 | .56264 | .3043 45 | .56263 | .3171 24 | .56234 |
| | 4705 | 106,251 | .9496 58 | .95771 | ----- | ----- | .9512 61 | .95617 |
| | 5462 | 91,540 | .1650 16 | .27092 | .1295 10 | .27109 | .1399 25 | .27071 |
| | 5792 | 86,324 | .9408 41 | .26787 | ----- | ----- | .9125 50 | .26796 |

*Integral part only.

**Fractional part only.

Table 3. Data From The 2.8 cm. Spacer.

| | Vacuum Wavelength (in Angstroms) | Interference Order Number* | Plate 7 | | Plate 8 | | Plate 9 | |
|-----------------------|--------------------------------------|----------------------------|-----------------------------|---------------------------------------|-----------------------------|---------------------------------------|-----------------------------|---------------------------------------|
| | | | Interference Order Number** | Double Plate Separation (in cm.) | Interference Order Number** | Double Plate Separation (in cm.) | Interference Order Number** | Double Plate Separation (in cm.) |
| Initial Neon Exposure | 5854.10979 | 95,634 | .4099 | 5.59854 355 | .4237 | 5.59854 416 | .4189 | 5.59854 388 |
| | 5946.48074 | 94,148 | .8565 | 362 | .8670 | 424 | .8604 | 385 |
| | 6219.00100 | 90,023 | .2035 | 393 | .2058 | 407 | .2115 | 442 |
| | 6268.22821 | 89,316 | .2154 | 421 | .2085 | 378 | .2214 | 459 |
| | | | Average: | 5.59854 378 | | Average: | | Average: |
| | | | | | | 5.59854 406 | | 5.59854 418 |
| Final Neon Exposure | 5854.10979 | 95,634 | .4192 | 5.59854 390 | .4206 | 5.59854 398 | .4151 | 5.59854 366 |
| | 5946.48074 | 94,148 | .85133 | 331 | .8638 | 405 | .8617 | 393 |
| | 6219.00100 | 90,023 | .2061 | 409 | .2088 | 426 | .2114 | 442 |
| | 6268.22821 | 89,316 | .2088 | 380 | .2118 | 398 | .2158 | 423 |
| | | | Average: | 5.59854 378 | | Average: | | Average: |
| | | | | | | 5.59854 407 | | 5.59854 406 |
| | | | Overall average: | 5.59854 378 | | Overall average: | | Overall average: |
| | | | | | | 5.59854 406 | | 5.59854 412 |
| | Vacuum Wavelength* (in Angstroms) | Interference Order Number* | Interference Order Number** | Vacuum Wavelength** (in Angstroms) | Interference Order Number** | Vacuum Wavelength** (in Angstroms) | Interference Order Number** | Vacuum Wavelength** (in Angstroms) |
| Mercury Exposure | 2537 | 220,652 | .4112 \pm .0052 | .26834 | .4146 \pm .0075 | .26843 | .4479 \pm .0066 | .26808 |
| | 2652 | 211,040 | .2248 72 | .83255 | .22239 59 | .83272 | .2023 70 | .83300 |
| | 2752 | 203,317 | .4531 22 | .59724 | .4827 41 | .59698 | .5013 13 | .59676 |
| | 2894 | 193,423 | .6542 62 | .44629 | .6600 75 | .44635 | .6620 74 | .44635 |
| | 2968 | 188,620 | .6961 71 | .14925 | .6875 30 | .14954 | .7001 58 | .14936 |
| | 3022 | 185,236 | .2942 58 | .37950 | .3051 53 | .37947 | .2998 \pm .0030 | .37959 |
| | 3024 | 185,115 | .1614 38 | .35724 | .1726 60 | .35720 | .1912 77 | .35693 |
| | 3126 | 179,063 | .1502 69 | .57505 | .1396 59 | .57539 | .1652 33 | .57498 |
| | 3342 | 167,498 | .6048 29 | .44204 | .6221 36 | .44186 | .6135 21 | .44207 |
| | 3651 | 153,334 | .5331 75 | .19564 | .5219 53 | .19608 | .5202 26 | .19616 |
| | 3655 | 153,138 | .0638 40 | .87996 | .0804 48 | .87974 | .0932 27 | .87948 |
| | 3664 | 152,785 | .1864 52 | .32369 | .1997 56 | .32355 | .2100 12 | .32335 |
| | 4047 | 138,313 | .7049 32 | .71442 | .7184 42 | .71423 | .7236 50 | .71412 |
| | 4078 | 137,253 | .2242 31 | .98890 | .2257 56 | .98906 | .2316 20 | .98893 |
| | 4359 | 128,419 | .8720 29 | .56188 | .8733 13 | .56205 | .8796 14 | .56188 |
| | 4705 | 118,967 | .1518 58 | .95765 | .1317 37 | .95868 | .1712 43 | .95717 |
| | 5462 | 102,494 | .7975 37 | .27118 | .8127 40 | .27064 | ---- | ----- |
| | 5792 | 96,655 | .4710 32 | .26786 | .4870 26 | .26719 | .4845 29 | .26740 |

*Integral part only.

**Fractional part only.

b. Phase Change Correction

Table 4. Correction for 1.5 cm. and 2.5 cm. Spacers

| Vacuum Wave- length* (in Ang- stroms) | Wavelength** at 1.5 cm. Spacer | | Wavelength** at 2.5 cm. Spacer | | Phase Change Correction to 2.5 cm. Spacer | | Corrected Wavelength** | |
|---|--------------------------------------|----|--------------------------------------|----|---|-----|---------------------------|-----|
| 2537 | .26867 ± .00016 | | .26871 ± .00006 | | +.00006 ± .00026 | | .26876 ± .00027 | |
| 2652 | .83311 | 2 | .83292 | 26 | -.00028 | 39 | .83264 | 46 |
| 2753 | .59730 | 29 | .59723 | 5 | 10 | 44 | .59713 | 44 |
| 2894 | .44638 | 11 | .44663 | 22 | +.00038 | 38 | .44701 | 44 |
| 2968 | .14941 | 11 | .14962 | 10 | 32 | 22 | .14994 | 23 |
| 3022 | .37961 | 5 | .37983 | 10 | 33 | 16 | .38016 | 19 |
| 3024 | .35751 | 22 | .35730 | 16 | -.00032 | 40 | .35698 | 43 |
| 3126 | .57521 | 13 | .57564 | 14 | +.00064 | 28 | .57628 | 31 |
| 3342 | .44188 | 11 | .44257 | 14 | 104 | 27 | .44361 | 30 |
| 3651 | .19580 | 30 | .19607 | 22 | 40 | 56 | .19647 | 59 |
| 3655 | .87948 | 13 | .88014 | 14 | 99 | 28 | .88113 | 31 |
| 3664 | .32360 | 15 | .32415 | 13 | 82 | 30 | .32497 | 33 |
| 4047 | .71412 | 22 | .71453 | 10 | 62 | 34 | .71515 | 35 |
| 4078 | .98864 | 29 | .98907 | 15 | 64 | 50 | .98971 | 52 |
| 4359 | .56233 | 30 | .56254 | 14 | 32 | 50 | .56286 | 52 |
| 4705 | .95779 | 45 | .95694 | 77 | -.00128 | 134 | .95566 | 160 |
| 5462 | .27092 | 27 | .27095 | 16 | +.00004 | 46 | .27099 | 49 |
| 5792 | .26743 | 28 | .26792 | 5 | 74 | 42 | .26866 | 42 |

*Integral part only

**Fractional part only

Table 5. Correction for 1.5 cm. and 2.8 cm. Spacers

| Vacuum Wave- length* (in Ang- stroms) | Wavelength** at 1.5 cm. Spacer | | Wavelength** at 2.8 cm. Spacer | | Correction to 2.8 cm. Spacer | | Corrected Wavelength** |
|---|--------------------------------------|----|--------------------------------------|----|------------------------------------|----|---------------------------|
| 2537 | .26867 \pm .00016 | | .26828 \pm .00015 | | -.00045 \pm .00025 | | .26783 \pm .00029 |
| 2652 | .83311 | 2 | .83276 | 19 | 40 | 22 | .83236 29 |
| 2753 | .59730 | 29 | .59697 | 20 | 38 | 40 | .59659 45 |
| 2894 | .44638 | 11 | .44633 | 03 | 06 | 13 | .44627 13 |
| 2968 | .14941 | 11 | .14942 | 12 | +.00001 | 18 | .14943 22 |
| 3022 | .37961 | 5 | .37953 | 06 | -.00009 | 09 | .37944 11 |
| 3024 | .35751 | 22 | .35715 | 14 | 42 | 30 | .35673 33 |
| 3126 | .57521 | 13 | .57510 | 18 | 13 | 25 | .57497 31 |
| 3342 | .44188 | 11 | .44200 | 09 | +.00014 | 16 | .44214 18 |
| 3651 | .19580 | 30 | .19601 | 22 | 24 | 43 | .19625 48 |
| 3655 | .87948 | 13 | .87969 | 20 | 24 | 28 | .87993 34 |
| 3664 | .32360 | 15 | .32348 | 15 | -.00014 | 24 | .32334 29 |
| 4047 | .71412 | 22 | .71427 | 12 | +.00017 | 29 | .71454 31 |
| 4078 | .98864 | 29 | .98895 | 07 | 36 | 35 | .98931 35 |
| 4359 | .56233 | 30 | .56195 | 08 | -.00044 | 36 | .56151 37 |
| 4705 | .95779 | 45 | .95795 | 65 | +.00018 | 91 | .95813 110 |
| 5462 | .27092 | 27 | .27091 | 27 | -.00001 | 44 | .27090 52 |
| 5792 | .26743 | 28 | .26748 | 28 | +.00006 | 45 | .26754 53 |

* Integral Part Only

** Fractional Part Only

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• (3.15) $\text{Hom}(V, W)$ is a vector space over F .

• $\text{Hom}(V, W)$ is isomorphic to $M_{n \times m}(F)$ if V has dimension n and W has dimension m .

• $\text{Hom}(V, W)$ is isomorphic to $M_n(F)$ if $V = W$ and V has dimension n .

• $\text{Hom}(V, W)$ is isomorphic to $M_n(F)$ if $V = W$ and V has dimension n .

• $\text{Hom}(V, W)$ is isomorphic to $M_n(F)$ if $V = W$ and V has dimension n .

• $\text{Hom}(V, W)$ is isomorphic to $M_n(F)$ if $V = W$ and V has dimension n .

• $\text{Hom}(V, W)$ is isomorphic to $M_n(F)$ if $V = W$ and V has dimension n .

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